

Role of cellulose nanocrystals in epoxy-based nanocomposites: mechanical properties, morphology and thermal behavior

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Abstract

This study evaluated the influence of cellulose nanocrystals (CNC) content on the properties of epoxy nanocomposites. The CNC were obtained from microcrystalline cellulose by acid hydrolysis. 4.0, 5.5 and 7.0% of untreated CNC were incorporated into epoxy resin. Sonication was used to disperse the CNC in the resin. The thermal stability, the glass transition temperature and the degree of conversion were reduced as observed by Thermogravimetry and Differential Scanning Calorimetry, respectively. The tensile and bending modulus showed no significant improvement and the impact resistance showed a slight reduction due to the non-uniform dispersion of the CNCs, as observed by Transmission Electron Microscopy. Analysis of Scanning Electron Microscopy showed a change of the fracture mechanism of the epoxy resin: the CNCs increased the elastic modulus by reinforcement, but accelerated the fracture by acting as defects. The Halpin-Tsai model was applied to predict the elastic modulus of the epoxy/CNC system.

Keywords: *cellulose nanocrystals, nanocomposites, epoxy resin.*

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1. Introduction

The development of high-performance polymers has focused on materials that are reinforced with nanoparticles that can improve the properties in relation to those made with pure materials. Polymeric nanocomposites are materials that contain fillers, in which at least one of their dimensions has measurements that is less than 100 nm, dispersed in a polymer matrix^[1]. They are part of a class of engineering materials that are very attractive because they provide better mechanical and thermal properties than conventional composites. In addition, only small amounts of reinforcement are required^[2,3]. Cellulose nanocrystals (CNCs) are one of these particles that are used because they have a set of peculiar characteristics that characterize them as a good polymer matrix-reinforcing agent. These characteristics are the following: a high amount of hydroxyl groups that can provide the possibility of very good interaction in the polymer/filler interface; a high specific surface area and high aspect ratio that is important to stress transfer; high crystallinity and elastic modulus, which are responsible for the increase in stiffness; as well as high thermal stability, low cost, low density and a peculiarly interesting morphology^[4].

Due to the excellent properties of CNCs, many studies have been developed that show their use as nanofillers in polymers. The high polarity and high hydrophilicity nature of CNCs causes the interaction and dispersion in some types of polymeric matrices to be compromised^[4]. Polar matrices can present better dispersion of the CNCs due to the high interaction of hydrogen bonds, thus obtaining better mechanical properties^[5], while nonpolar matrices can present worse dispersion and reduced mechanical properties.

Many studies have shown that CNC surfaces treated with organic compounds have a better interaction with non-polar polymers^[6]. However, in order to promote better interaction with the polymeric matrix, treated CNCs are used in liquid suspension^[7]. Another factor that influences the dispersion of CNCs in the polymer matrix is the method used for obtaining it. Some methods of obtaining nanocomposites use complex equipment such as extrusion and hot pressing^[7]. In this study, the CNCs were inserted in the polymeric matrix in the form of a dry powder and the nanocomposites were obtained by a simple method of manual mixing at room temperature.

CNCs are extracted from cellulose, which is the most abundant natural polymer in nature. Among other sources,

they can be extracted from microcrystalline cellulose (MCC), which is a substance obtained from partially depolymerized cellulose. It can be dried to a fine, powdery particle form or co-processed with a water-soluble polymer to form a colloid. MCC is widely used because it is chemically stable and physiologically inert^[8]. As such, there has been increased interest in its use in the pharmaceutical^[9], food industries and the energy sector^[10].

Epoxy resin was chosen as the nanocomposite matrix for this study. Epoxy resin is part of an important class of high-performance thermosetting polymers that are widely used in automotive, construction and aerospace applications^[11]. It is considered one of the best matrices since it has excellent properties such as good adhesion^[12], good mechanical properties such as high elastic modulus, shear strength, corrosion resistance, thermal stability, low shrinkage after the curing process, favorable viscosity properties, light weight, low cost, resistance to environmental degradation, as well as good friction and wear resistance^[13].

The incorporation of CNCs in the epoxy resin can result in a high stiffness and good fatigue strength, which, for example, is very desirable in aerospace applications. Studies in which CNCs from tunicates and cotton were incorporated into the epoxy matrix showed good dispersion and consequent improvement in mechanical properties due to the increased in interfacial adhesion between the CNCs and the epoxy matrix^[14].

Roszowska-Jarosz et al.^[15] describe the production of epoxy/CNC nanocomposites by adding a suspension of CNCs and acetone in the quantities of 0.5%, 1% and 1.5%wt in epoxy resin, for which they obtained superior values for impact resistance and flexural strength. Nissilä et al.^[16] produced nanocomposites by impregnating cellulose nanofibers (CNF) in bio-epoxy resin. For this, they produced suspensions in water in the quantities of 1.0 and 1.5%wt of CNF and then they prepared aerogels by freezing the suspensions in molds. The frozen suspensions were impregnated with the bio-epoxy resin using a vacuum and its curing was carried out at 80 °C. Data on the mechanical properties were obtained by tensile and flexion tests in which the nanocomposites showed an increase in the flexural modulus of approximately 50%, and of 20% in the tensile strength in relation to the polymer without CNF. Qi et al.^[17] produced CNC/epoxy nanocomposites using superficially modified CNCs by grafting with poly (n-vinylpyrrolidone), which significantly increased the toughness of epoxy resin and is explained by the excellent dispersion of the CNCs and its effect in promoting plastic deformation in the system. Some other works mention the modification of epoxy resin with CNCs identifying, in addition to changes in mechanical properties, changes in thermal characteristics^[18].

The objective of this study was to characterize the CNCs obtained from MCC and evaluate the mechanical properties of epoxy/CNC nanocomposites considering the influence of the CNC volumetric fraction, taking into account fractions in above, and below the percolation threshold. The Halpin-Tsai modulus of elasticity prediction model was applied as a tool to understand the interactions of the components and the mechanical behavior of the system under study.

2. Material and Methods

2.1 CNC production

Commercial microcrystalline cellulose (MC 500, Blanver, Brazil) was used as a source of cellulose for CNC extraction. Sulfuric acid (Synth) was used in the acid hydrolysis process. The nanocomposites were produced using DER 331 bisphenol A diglycidyl ether-based (DGEBA) epoxy resin and the hardener DEH 24, a triethylenediamine (Dow Chemical Company), which were mixed in the ratio of 100:13, as indicated by the supplier.

Acid hydrolysis consists of a process that removes the amorphous phase of cellulose so that the nanocrystals are isolated. Microcrystalline cellulose was hydrolyzed with sulfuric acid solution (55% v/v) at 45 °C for 30 min under constant stirring, then, 300 mL of distilled water was added to stop the reaction, following the Hassan method^[19]. The ratio was 10 mL of sulfuric acid solution to 1 g of microcrystalline cellulose.

Centrifugation was applied to partially remove sulfuric acid and separate the nanocrystals from the solution. The supernatant that appeared after 10 minutes of each centrifugation cycle at 6000 rpm was removed and replaced with distilled water. This exchange procedure was performed repeatedly until the solution reached a pH close to 7. The resulting suspension was submitted to dialysis. The material was placed on the dialysis membrane so that the exchange with the aqueous medium occurred. The water, where the membranes were immersed, was replaced once after 24 h and dialysis continued for a further 24 h. As the last step, lyophilization consisted of the total removal of water using a freeze dryer, which left only the powdered nanocrystals. From this step, the CNCs were ready to be incorporated into the epoxy matrix. During this stage, CNCs tend to cluster together in structures that are stabilized by hydrogen interactions. Freeze-drying was the method of drying used, and this allows the dispersed CNC material structure to be maintained.

2.2 Nanocomposites production

Nanocomposites with a CNC volumetric concentration of 4.0, 5.5 and 7.0% were prepared. These concentrations were determined from the theoretical calculation of the percolation threshold^[20]. The CNCs were weighed and carefully added to the epoxy resin, then manually mixed at room temperature, according to the work of Omrani et al.^[21]. An ultrasonic probe (QSONICA, Q700, USA) was used with a maximum power of 700 W and a 6.4 mm diameter sonotrode for 10 min. To fully disperse the CNCs in the polymer matrix under 30 W power conditions. Then, the hardener was added and mixed evenly with the resin. Figure 1 shows a schematic of the steps in the production of nanocomposites. The mold used was produced in aluminum alloy with dimensions of 30 × 30 × 1.5 cm and its cavities in the shapes and dimensions of specimens for mechanical tests were produced by machining (Figure 2). As a release agent, PVC film was used inside the mold. The mixture was poured into the mold and kept at room temperature at atmospheric pressure for curing.

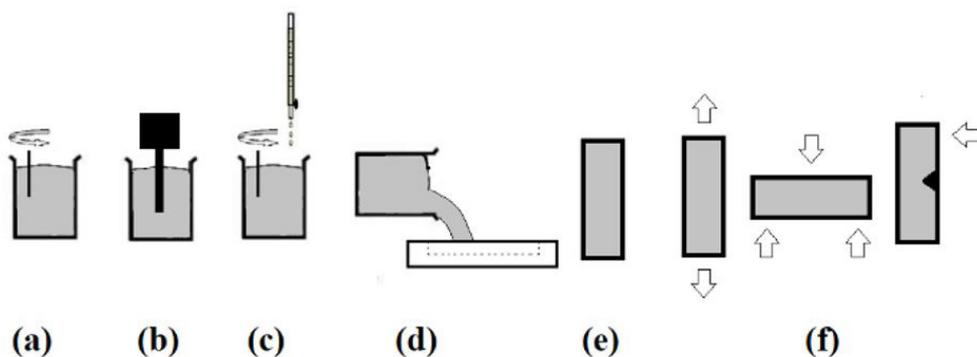


Figure 1. (a) Manual mixing of CNCs and epoxy resin; (b) ultrasonic CNC dispersion; (c) manual addition and mixing of hardener; (d) the mixture poured into the mold; (e) specimen after curing and (f) mechanical testing.

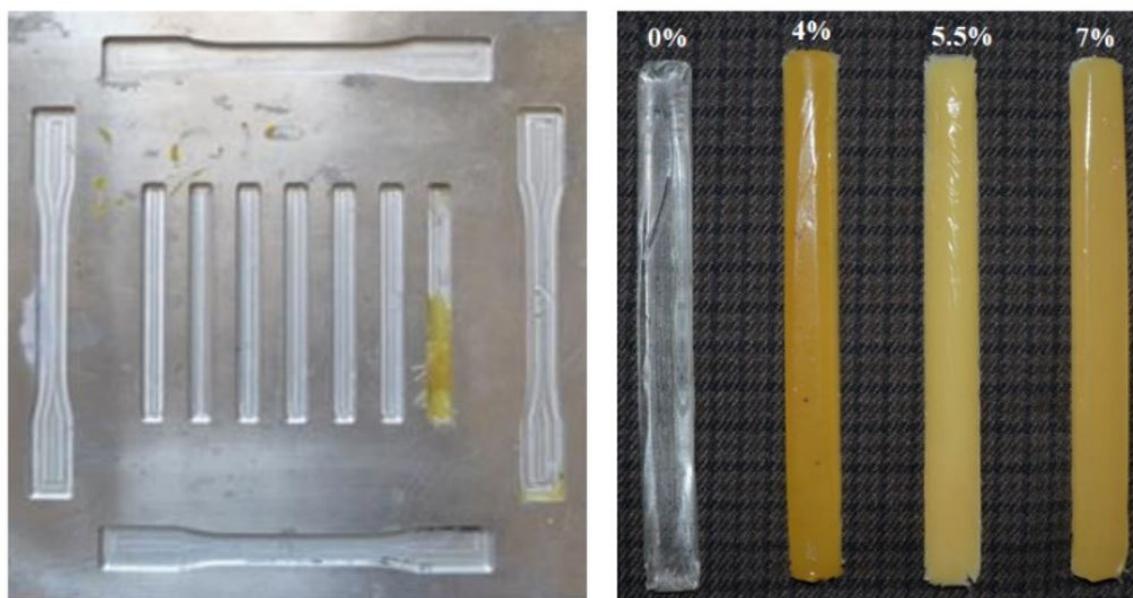


Figure 2. Metal mold and specimens produced.

2.3 CNCs and nanocomposite characterization

The samples of CNCs obtained were analyzed by using Fourier transform infrared spectroscopy (FTIR) (Nicolet 6700, Thermo Scientific, USA). The spectra were obtained in the ATR mode, with the SMART OMNI-SAMPLER accessory operating in the 4000-675 cm^{-1} range, with 4 cm^{-1} resolution and 128 scans.

Transmission electron microscopy (TEM) (JEM 2100, JEOL, Japan) was used to evaluate the morphology of the CNCs. To obtain the TEM image, a drop of the diluted CNC suspension was allowed to dry on a carbon-coated copper grid (400 mesh). To improve contrast, a 2% by weight solution of uranyl acetate was placed on the grid for 30 seconds.

For determination of the aspect ratio (L/D), dimensions of the CNCs were obtained from TEM images with the aid of Image J software. For this calculation, about 60 units of CNCs were used.

The crystal structure of the CNCs was evaluated using X-ray diffraction analysis (XRD), (X'Pert-MPD, Philips, USA), operating with $\text{CuK}\alpha$ ($\lambda = 1.54060 \text{ \AA}$), 40 kV voltage and 40 pA current, 2θ between 5 and 50° . The samples were placed in the XDR equipment in dry powder form. The degree of crystallinity was estimated following the method cited by Martin et al.^[22] as it is widely used for natural fibers. The index (I_c) was estimated by means of Equation 1.

$$I_c = 1 - \left(\frac{I_{\text{am}}}{I_{002}} \right) \times 100 \quad (1)$$

Using the peaks (I_{002} , $2\theta = 22.4^\circ$) and (I_{am} , $2\theta = 18.8^\circ$), I_{002} represents both the crystalline and the amorphous material, while I_{am} represents amorphous material.

The nanocomposites obtained were analyzed using FTIR (Nicolet 6700, Thermo Scientific, USA). Infrared spectra were obtained in ATR mode, with the SMART OMNI-

SAMPLER accessory operating in the 4000-675 cm^{-1} range, with 4 cm^{-1} resolution and with 128 scans.

To evaluate the thermal behavior, DSC equipment (DCS1, Mettler Toledo, Switzerland) was used with a heating rate from 10 $^{\circ}\text{C}/\text{min}$ from -30 to 300 $^{\circ}\text{C}$ and an inert atmosphere (N_2) with a flow of 50 ml/min. Firstly, the total cure enthalpy of the base system was obtained from the DSC analysis of the resin + hardener in the range of -30 to 300 $^{\circ}\text{C}$ in the proportions indicated by the manufacturer, which was found to be 4592 mJ.

The nanocomposites were also evaluated using a thermogravimetric analyzer (TG) (TGA-50M, Shimadzu, Japan) and a microanalytical scale (MX5, Mettler Toledo, Switzerland). Analyses were performed in an inert atmosphere (N_2), in a temperature range of 25 to 600 $^{\circ}\text{C}$, and a heating rate of 10 $^{\circ}\text{C}/\text{min}$.

The morphology and size distribution of the particles in the CNC filled epoxy nanocomposites were studied by using TEM (TECNAI T20, FEI, USA) with 200 kV. In this analysis, the samples with 4.0, 5.5 and 7.0% of CNCs was cut in thin sections (around 120 nm in thickness) using an ultramicrotome (UltraCut, Leica, Austria) and placed on a copper grid of 3 mm in diameter.

A universal testing machine was used to obtain the tensile mechanical properties of modulus of elasticity (E_T), tensile strength (σ_T) and strain at break (ϵ_T). Samples were prepared according to ASTM D638-10, Type I, and an extensometer (High Elongation extensometer AHX850, MTS, USA) was used. For each formulation, five specimens were tested and the average value was calculated. The universal test machine (Alliance RT/5, MTS, USA) operated at a crosshead speed of 1 mm/min and a 5 kN load cell was used.

Flexural tests of the samples were performed and flexural modulus (EF) and flexural strength (σ_F) were evaluated. For each formulation, five specimens were tested and the average value was calculated. The 3-point bending tests were performed at room temperature according to ASTM D790-03. A universal testing machine (5984, Instron, USA) was used with a 150 kN load cell and at speed of 2 mm/min.

For determination of the impact strength (IS) the samples were prepared according to ASTM D4812-19 and

the notched Izod test was performed using an impact tester (Impact 104, Tinius Olsen, USA) with capacity of 25 J and a 10 $^{\circ}$ impact hammer.

The nanocomposite fractured surface morphology was studied using scanning electron microscopy (SEM) (LEO 440i, Leica, England) at 10 mA operating current.

The samples from the tensile test were cut at 5.0 mm (manual cutter) below and parallel to the fracture. The cut piece was fixed with carbon adhesive on the SEM sample holder and was gold sputter coated with a sputter coater (SC7620, Polaron VG Microtech, UK) with a film of approximately 20-50 nm.

3. Results and Discussion

3.1 CNC characterization

Figure 3 shows the comparative FTIR spectra of the MCC and the CNCs. In the MCC spectrum, the band around 3400 cm^{-1} , which is due to the OH-stretching vibration, is typical for adsorbed water and gives considerable information concerning the hydrogen bonds. The band at 2900 cm^{-1} corresponds to the stretching of the C-H bonds. The bands at 1430, 1059 and 897 cm^{-1} are typical of pure cellulose and can be seen in both the MCC and CNC spectrum. In general, the 897 cm^{-1} band is assigned to vibrations of the C-O-C elongations of the characteristic β (1 \rightarrow 4) glycosidic bond^[23]. Therefore, typical cellulose bands can be seen in both the MCC and CNCs^[24].

Figure 4 shows the results of X-ray diffraction of the CNCs and the MCC. A peak at 22.42 $^{\circ}$ can be observed and indicates the presence of crystallinity that is characteristic of this nanoparticle. This peak refers to cellulose type I and approaches the value of 22.7 $^{\circ}$ found in the literature^[25]. This means that the CNCs were isolated from other parts of the cellulose and that the acid hydrolysis process did not change their structure during treatment. The degree of crystallinity obtained was 82.7%. The degree of crystallinity was calculated following the method cited by Martin et al.^[22] and is widely used for natural fibers. One shoulder can also be observed on the diffractogram around 20 $^{\circ}$, which refers

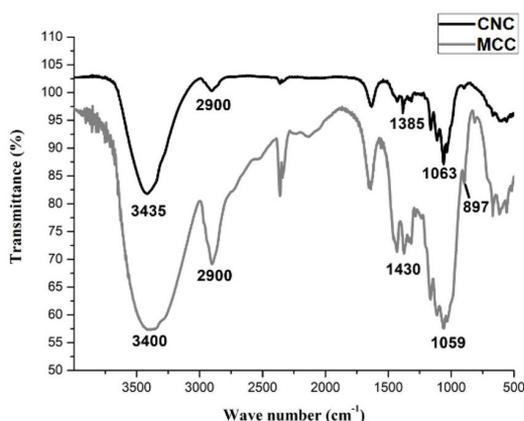


Figure 3. CNC and MCC FTIR spectra.

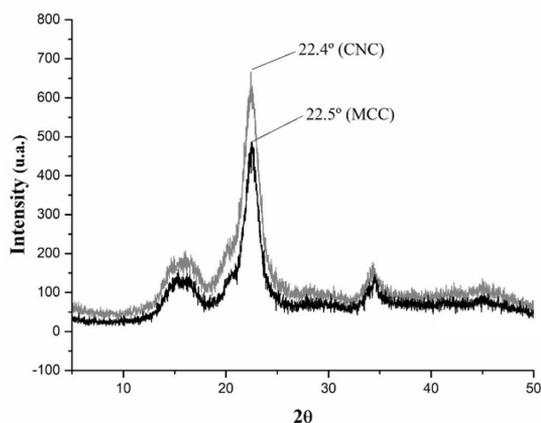


Figure 4. Diffractogram of the CNCs and the MCC.

to cellulose type II that could be present in low amounts. At peak 22.5° of the MCC, a lower intensity is observed and this may indicate the presence of amorphous regions^[26].

Figures 5a-c show the image from the TEM that was performed after the CNCs were lyophilized. It can be observed that the nanocrystals were obtained successfully. The image shows the needle-like nanoparticles that correspond to the characteristic and expected morphology of the CNCs. It can also be noted that there was some level of agglomeration of particles and consequent stacking on each other. The CNC agglomeration phenomenon is mainly due to their very small size and their very high surface energy. In addition, the hydroxyl group on the surface of the CNCs facilitates the formation of hydrogen bonds, which facilitates their approximation.

The morphology of the CNCs is shown in Figure 5. The length (L) and diameter (D) of the CNCs were (142±36) nm and (11±2.5) nm, respectively. A total of 60 length and diameter measurements were taken and then the aspect ratio (L/D) was calculated from each measurement. Thus, the aspect ratio obtained was 12.5. A high aspect ratio results in high rigidity of the percolated nanoparticle network and this favors the reinforcing effect on a nanocomposite since a good dispersion is obtained in polymer matrices. In order to have a good transfer of tensions between the matrix and the reinforcement, the minimum value of the aspect ratio must be 10^[27], which was obtained in this work however, other aspects, such as the compatibility between the matrix and the dispersed phase, the percolation limit and the dispersion, must be considered^[20]. CNCs have a tendency to aggregate, as seen in Figure 5.

3.2 Nanocomposite characterization

In order to understand the relationship between processing, morphology, properties and durability of a thermoset material and, consequently, of the composite, it is necessary to understand the cure mechanism of the system. Table 1 summarizes the DSC data. T_g values of the nanocomposites were reduced by 5 °C for the samples with 5.5 and 7.0% of CNCs in relation to pure epoxy. Residues of water molecules on the surfaces of CNC aggregations may have affected the crosslinking of the epoxy matrix^[28].

As T_g was influenced by the presence of the CNCs, it can be assumed that the nanocomposite can be processed under the same conditions as the neat system and that the thermal behavior under the application conditions would be close.

The samples were cured at room temperature. An important point is that, for all samples, the relaxation enthalpy was observed and the cure was not complete. The conversion for each sample was determined following the method of Hardis et al.^[29]. The values are shown in Table 1, in which it is observed that the conversion is very similar for all samples, although the presence of (-OH) groups of cellulose may participate in the curing reaction of the epoxy resin and result in increased conversion^[29]. It is possible that this effect was diminished by the spatial restriction caused by the CNCs.

In order to understand the chemical structure of epoxy resin and especially nanocomposites in more detail, the FTIR spectra were evaluated. Figure 6 shows the spectra of epoxy and nanocomposites with different CNC contents. The epoxy group has three characteristic absorption bands in the infrared spectrum. One is the band appearing in the 1250 cm⁻¹ range, which corresponds to the symmetrical axial deformation of the epoxy ring and the aromatic ether group C-O-C, in which all its bonds expand and contract in phase^[30]. Another is the 916 cm⁻¹ band, which is related to the asymmetric axial deformation of the ring, in which the C-C bond increases and the C-O bond contracts. The third band appears in the 840-750 cm⁻¹ range and corresponds to the C-O-C bond^[31]. The absorption present in the 3000-3500 cm⁻¹ range refers to the hydroxyl groups of adsorbed water that were identified in all the nanocomposites. The absorption around 2925 cm⁻¹ is due to the stretching of C-H

Table 1. Results of thermal analysis: glass transition temperature (T_g), residual enthalpy (ΔH_R) and conversion degree (X).

*V CNC (%)	T _g (°C)	ΔH_R (mJ/mg)	X (%)
0	67	123	97
4	67	182	96
5.5	63	249	95
7	63	243	95

*CNC volumetric concentration (%).

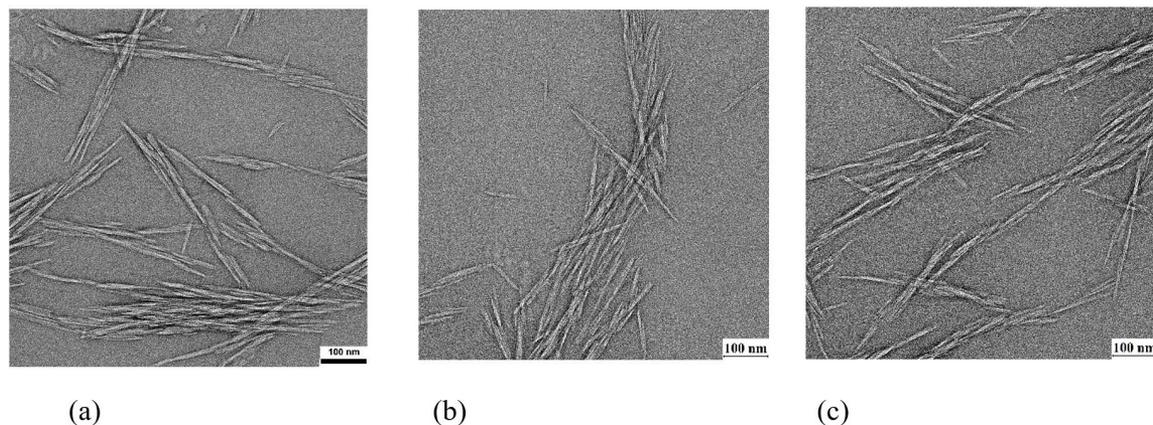


Figure 5. (a), (b), (c) Transmission electron micrographs of the obtained CNCs.

bonds. Strong absorptions between 1000 and 1250 cm^{-1} indicate the C-O-C (ether) or C-O-H groups. The bands in the 2900-2930 cm^{-1} range indicate stretching of C-H bonds. Monitoring the band at 916 cm^{-1} allowed us to evaluate the existence of residual epoxy groups, which indicate if the cure was complete with the consumption of most groups. As can be seen in Figure 6, this band almost disappeared in the nanocomposite spectra. This means that there was a small cure residual, as observed in the DSC analysis. All the CNCs/epoxy nanocomposites at different filler loadings displayed similar FTIR spectra.

The interfacial interaction of the CNCs and epoxy resin can be evaluated using FTIR. A reduction in bands between 3000-3500 cm^{-1} was observed for nanocomposites. These bands refer to the hydroxyl groups adsorbed on the surface of the CNCs. This behavior indicates that there may have been a low interfacial interaction between the CNCs and the epoxy in the production of the nanocomposites^[17], although the CNCs were expected to be trapped in the cross-linked epoxy resin and completely covered by the polymer chains via hydrogen bonds^[18]. The TEM images confirm the low interaction and, as a consequence, the formation of clusters. This low interaction may have affected the mechanical and

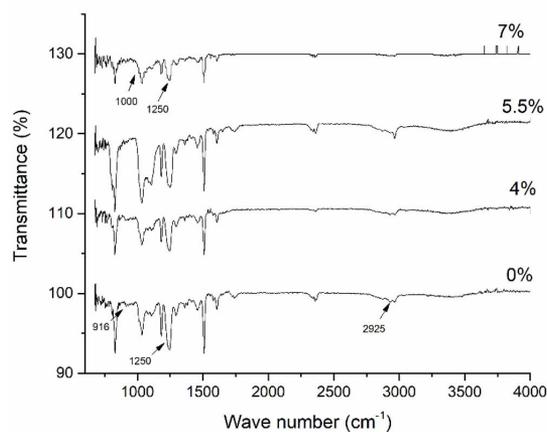
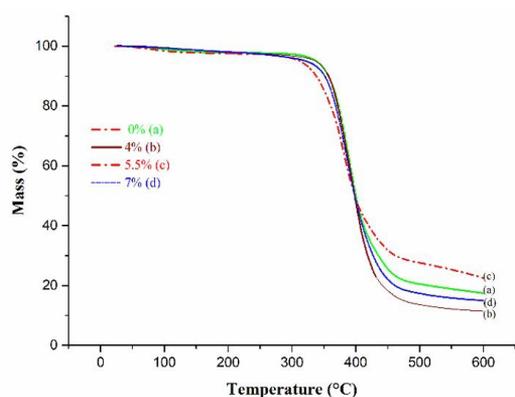
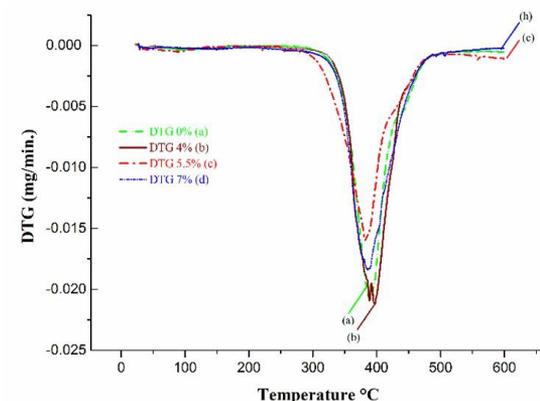


Figure 6. FTIR spectra of pure epoxy resin and nanocomposites.



(a)



(b)

Figure 7. (a) TG curves and (b) Derivative TG analysis of pure epoxy resin and nanocomposites.

thermal properties of the nanocomposites, making them inferior to CNC-free epoxy and this will be discussed later.

The thermal stability of the pure epoxy resin and the nanocomposites was evaluated using TG analysis. Figure 7 shows the degradation temperature curves, and the results are presented in Table 2. It is observed that there was an initial mass reduction for temperatures between 50-200 $^{\circ}\text{C}$, which was due to moisture loss from the dehydration of secondary alcoholic groups and the evaporation of physically weak and loosely bound moisture on the surfaces of the composites^[32].

Table 2 shows that the moisture loss was greater for the nanocomposites than for the pure epoxy. This behavior suggests that the CNCs adsorbed water on their surface. It was also observed that the moisture loss values are close to those of the nanocomposites, which suggests that the amount of water did not increase when the CNC fractions increased. The interaction of the epoxy resin matrix acted as a water barrier that prevented the attraction with the hydrophilic hydroxyls on the surface of the CNCs. CNC aggregations in the epoxy matrix may also have prevented access to water on the surface of the CNCs^[33].

Thermal decomposition of pure epoxy resin occurs in two stages^[34]. The main mass loss occurs in the range of 300 to 500 $^{\circ}\text{C}$, which involves two stages of degradation. The initial loss peak around 350 $^{\circ}\text{C}$ corresponds to the degradation of the aliphatic amine curing agent due to its low C-N bond breakage energy. The second peak occurs in the temperature range of 405 $^{\circ}\text{C}$ and is attributed to resin decomposition^[18].

Table 2. Results of the TG analysis.

VCNC (%)****	T _{moisture loss} ($^{\circ}\text{C}$)	Moisture loss (%)	T _{onset} * ($^{\circ}\text{C}$)	T _{5%} ** ($^{\circ}\text{C}$)	T _{max} *** ($^{\circ}\text{C}$)
0	58-150	1.9	356	338	390
4	62-205	2.2	354	336	397
5.5	44-126	2.1	344	312	382
7	65-200	2.0	353	319	387

T_{onset}*: the onset temperature of weight loss; T_{5%}** : the temperature corresponding to 5% of weight loss; T_{max}***: the temperature corresponding to the maximum decomposition rate; ****VCNC volumetric concentration (%).

Comparing the TG analysis curves of the pure epoxy system with the nanocomposites, it can be observed that the thermograms are similar. No specific degradation step of the CNCs is observed in the nanocomposite thermograms, regardless of the volumetric concentration.

It was observed for the nanocomposites that as the CNC content increased, all initial degradation temperatures decreased in relation to the pure epoxy. The $T_{5\%}$ for the pure epoxy was 338 °C, and this was reduced when CNCs were added for the range of 336 to 319 °C. This behavior has already been described in the literature, in which T_{onset} is around 320 °C and it decreased when CNCs were added to the epoxy matrix, and is due to the lower T_{onset} temperature of the CNCs, which is around 230 °C^[17,35]. Moreover, for T_{max} , there was no relevant difference between the pure epoxy and the nanocomposites. Some of the divergent results due to the addition of CNCs can be explained by a complex energy dissipation mechanism of the interfaces between the nanocrystals and the matrix^[19]. The 5.5% nanocomposite, which corresponds to the percolation threshold volume fraction, presented the lowest thermal stability of all samples. The slight decrease in T_{max} for the 5.5 and 7.0% nanocomposites may have been due to increased thermal conductivity of the samples with the addition of the CNCs^[36,37].

3.3 Mechanical testing

There are many factors that directly affect the mechanical properties of nanocomposites, such as the inherent properties of the matrix and fillers, preparation conditions, interfacial adhesion (matrix-filler interaction), nanoparticle dispersion quality, and their concentration, which must be above the percolation threshold. Table 3 shows the results of the following mechanical properties: tensile modulus (E_T), flexural modulus (E_F), elongation in tensile (ϵ_T), elongation in flexural (ϵ_F), tensile strengths (σ_T), flexural strengths (σ_F) and impact strength (IS). The values of the modulus, the tensile strength and deformation for the tensile and flexural tests of the neat DGEBA/DEH24 are in accordance with other work in the literature^[38], but differ from those shown for the standard material^[39], which has a higher flexural modulus of 3.0 GPa and lower tensile strength of 79 GPa. Table 3 also shows that the nanocomposites' tensile modulus and flexural modulus values were higher than that of the neat epoxy. This behavior indicates that the high surface area of the CNCs and the presence of O-H groups in their surface caused, at a certain level, good interaction of the CNCs with the epoxy resin molecules^[17], and includes possible chemical bonding between the CNCs and the epoxy matrix^[40]. The values of elongation and tensile and flexural strengths have a tendency to reduction with the increase in the CNC concentration. Two main factors can explain this behavior: 1) the surface characteristics of the CNCs are an important

issue in order to improve the mechanical properties, and in some cases their modification can be suggested^[41] and 2) the dispersion must ensure the availability of the surface for an adequate transfer of mechanical stress from the matrix to the filler. CNCs have a rigid nature and a tendency to form agglomerates that act as micro-particles distributed in the epoxy matrix, which caused stress concentration points in the epoxy matrix and made it rigid and hard^[14,42]. Then, as the fraction of CNCs increased, the distribution of these agglomerates in the matrix also increased, and this caused the tensile and flexural moduli to increase, although in a lower proportion than expected. Furthermore, the agglomerates act as defects causing a premature fracture that reduces the elongation and strength. The TEM images shown in Figures 8a-c confirm the presence of the agglomerates in the nanocomposites.

The impact energy values for the nanocomposites were lower than those of the neat epoxy and the values decreased with the increase in the concentration of CNCs up to the concentration of 5.5% and, for the 7% concentration, there is a certain recovery in this property. This is in accordance with the results for the tensile and flexural values.

3.4 Mechanical model for elastic modulus prediction

Mechanical models help to validate experimental data. Most of them assume full or partial bonding between the reinforcement filler and the matrix. Among the best known for predicting the modulus of elasticity are the Mori-Tanaka models (based on the theory of inclusion and Eshelby's inclusion) and the Halpin-Tsai method (an interpretation of the Hill Potential theory). The latter is the most widely used to predict the modulus of elasticity of composites and

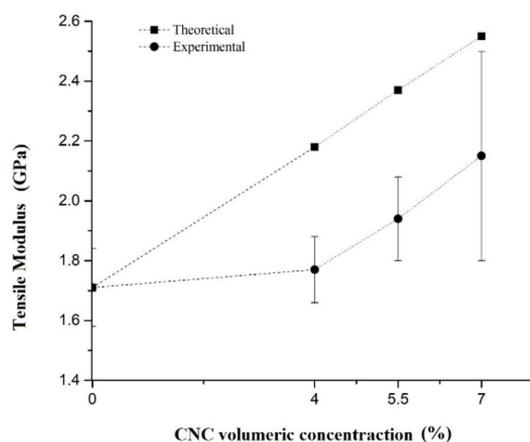


Figure 8. Theoretical and experimental tensile modulus of nanocomposites with different volume fractions.

Table 3. Mechanical properties of neat epoxy and nanocomposites.

V CNC (%) [*]	E_T (GPa)	σ_T (MPa)	ϵ_T (%)	E_F (GPa)	σ_F (MPa)	ϵ_F (%)	IS (J/m)
0	1.70 ± 0.13	96 ± 23	2.7 ± 0.9	1.60 ± 0.15	73.2 ± 1.8	3.2 ± 0.8	4.8 ± 0.3
4	1.77 ± 0.11	62 ± 12	2.0 ± 0.1	2.30 ± 0.01	61.6 ± 3.1	3.5 ± 0.1	3.9 ± 0.1
5.5	1.94 ± 0.14	57 ± 12	1.5 ± 0.6	1.90 ± 0.17	50.6 ± 10.8	3.1 ± 0.8	3.7 ± 0.6
7	2.15 ± 0.35	51 ± 15	1.3 ± 0.6	2.10 ± 0.13	67.6 ± 8.5	3.3 ± 0.2	4.3 ± 0.3

^{*}CNC volumetric concentration (%).

is a relatively simple universal model that can be applied to various compounds^[43]. In addition, it obtains and considers the form and aspect ratio of the reinforcement. The modified Halpin-Tsai model is presented in Equation 2. Coleman et al.^[44] states that this model provides better prediction of elastic modulus for low volumetric fractions.

$$E_c = \frac{3}{8} \frac{1+2\left(\frac{l_f}{d_f}\right) n_L V_f}{1-n_L V_f} E_m + \frac{5}{8} \frac{1+2 n_T V_f}{1-n_T V_f} E_m \quad (2)$$

In which: E_c : elastic modulus of composites. E_m : elastic modulus of epoxy matrix. E_f : elastic modulus of fiber. l_f = average fiber length. d_f = average fiber diameter, n_L = longitudinal efficiency factor and n_T = transverse efficiency factor according to Equations 3 and 4, respectively.

$$n_L = \frac{\left(\frac{E_f}{E_m}\right) - 1}{\left(\frac{E_f}{E_m}\right) + 2\left(\frac{l_f}{d_f}\right)} \quad (3)$$

$$n_T = \frac{\left(\frac{E_f}{E_m}\right) - 1}{\left(\frac{E_f}{E_m}\right) + 2} \quad (4)$$

This model is useful for predicting the behavior of unidirectionally aligned composite materials and is used to evaluate the reinforcing effect of randomly oriented nanoparticles. It assumes that the dispersion of nanoparticles is uniform. Considering the dimensions obtained for the studied CNCs, they showed the necessary conditions for acting as reinforcement. According to the Halpin-Tsai model, the higher the aspect ratio, the larger the composite modulus. Figure 8 shows the theoretical and experimental results. Although the behavior of the experimental data is similar to the theoretical one, values are lower than those expected for nanocomposites, which shows that the studied system failed in some aspects. To elucidate this behavior, microanalyses are further discussed.

In addition to the Halpin-Tsai prediction model being used to calculate the modulus of elasticity, it was also used to estimate the form factor (ξ). Since the elastic moduli of the components are known (Table 4), it was possible to theoretically evaluate the quality of the dispersion of the CNCs in the epoxy matrix. The form factor (ξ) was derived from the Halpin-Tsai model in order to be applied to the nanocomposites. This model predicts E_c/E_m (where E_c is the composite modulus and E_m is the matrix modulus) and the value of ξ for the best fit with the experimental results. The higher the value of ξ , the greater the indication of improvement in dispersion quality caused by the tendency of the nanoparticles to agglomerate^[46].

Figure 9 and Table 4 show that the dispersion quality is higher for smaller volume fractions. As can be seen, the proximity of the line of the experimental relative modulus is greater for $\xi = 10$. As the volumetric fractions of the CNCs increase, the quality of the dispersion decreases. The dispersion of nanoparticles is a crucial factor for

improving the resistance properties. This may explain the mechanical properties. The sample with 4% and 5.5% of CNCs showed better dispersion according to the model, which may justify this sample having greater rupture stress than the samples with larger volumetric fractions of CNCs. Therefore, where there is better dispersion, there is also an increase in rupture stress^[45].

Figures 10a-c shows the TEM images of the epoxy/CNC nanocomposites. The presence of the CNCs can be observed at various scales, as well as their dispersion in the epoxy matrix. The images show aggregations of CNCs in all the nanocomposites, as well as their non-uniform dispersion in the matrix. Ultrasound was applied in order to favor the dispersion of the CNCs in the matrix; however, the dispersion was not uniform and had the formation of aggregations, which may explain the poor performance regarding the mechanical properties in relation to the neat matrix. Uniform and good dispersion of the CNCs in the matrix tends to improve mechanical properties and tends to make the percolation theory applicable^[47]. Figure 10d shows an image with a greater magnitude of CNC aggregations in the epoxy matrix, and it is possible to observe its morphology.

The lack of a better reinforcing effect could be explained by the hydrophilic nature of CNCs^[40], which causes them to

Table 4. Values of the tensile modulus of the composites, matrix and CNCs.

Vf (4% CNCs)	Vf (5.5% CNCs)	Vf (7% CNCs)
Ec (GPa)		
1.77	1.94	2.14
Ec/Em ($\xi = 5$)		
1.11	1.16	1.20
Ec/Em ($\xi = 10$)		
1.07	1.10	1.14
Experimental		
1.03	1.13	1.25
E_{CNC} (GPa)		E_m (GPa)
50 ^[55]		1.70

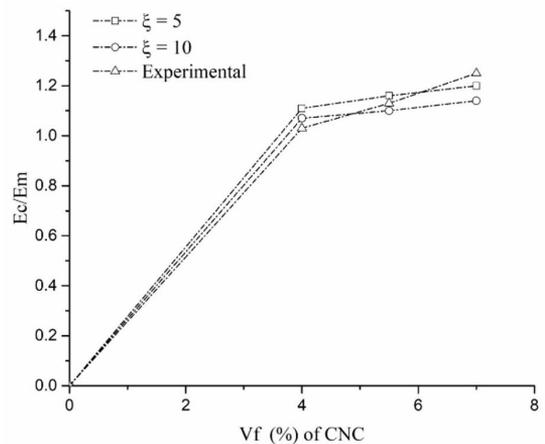


Figure 9. Comparison of experimental data with those predicted for the effect of Vf (CNCs) (fraction of volume in percentage) on the relative modulus of epoxy nanocomposites + CNCs.

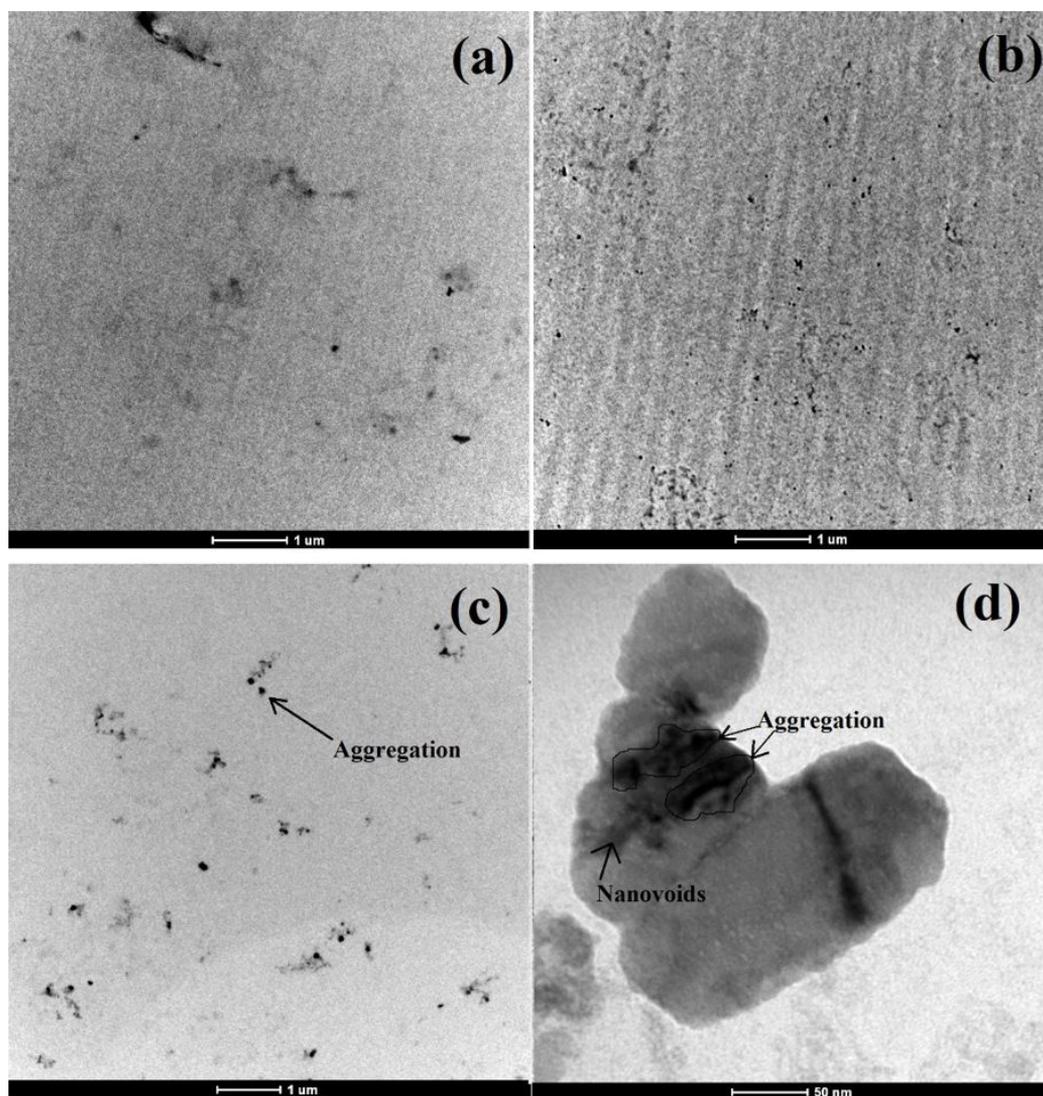


Figure 10. TEM images of nanocomposites (a) 4% CNCs, (b) 5.5% CNCs, (c) 7% CNCs, (Magnitude of 40,000 X) and (d) details of aggregation of CNCs (4% CNCs) (Magnitude of 200,000 X).

have a poor interaction with the epoxy matrix^[33,42]. Besides the lack of dispersion, the presence of water in the structure of the epoxy matrix can greatly affect the mechanical properties of nanocomposites^[48]. The slight reduction in the T_g values of the nanocomposites (5 °C for the 5.5 and 7% CNCs) shows that residues of water molecules on the surfaces of the CNC aggregations may have caused cellulose degradation. The molecules resulting from the degradation increased the free volume of the network structure of the epoxy matrix and, consequently, reduced the mechanical properties of the nanocomposites^[28]. The presence of CNCs in the epoxy matrix may also have hindered the crosslinking of the epoxy resin^[49], though the conversion was quite similar for all samples, which leads us to disregard this effect.

The samples with 7% CNCs showed that, even with the CNC aggregation, it may also have had better dispersion of CNCs and a better interfacial interaction with the matrix, and this led to greater toughness (IS) when compared to

other nanocomposites. The reduction of impact energy for nanocomposites is explained by the same reason, i.e., the CNC aggregations^[42,50].

The SEM images in Figures 11a-h show the effect of the CNCs on the fractured surfaces of the tensile tested samples. Neat epoxy resin (Figure 11a) has a smooth, homogenous and glassy region and semi-elliptical marks and steps^[51]. The surface pattern indicates a low resistance to crack propagation that led to brittle failure^[52]. The behavior in Figure 11b, marked by a black arrow, revealed its typical brittle nature with poor resistance to cracking or rupturing and its tendency towards propagation^[53,54]. Figures 11c-h show the SEM micrographs of the nanocomposites with 4.0, 5.5 and 7.0% CNCs. The incorporation of CNCs caused the roughness in the nanocomposite fractures observed in Figures 11c, e, and g. In the images, the black arrows show that the CNCs increase the roughness, similar to what was observed by Kumar et al.^[40]. Based on the images and on

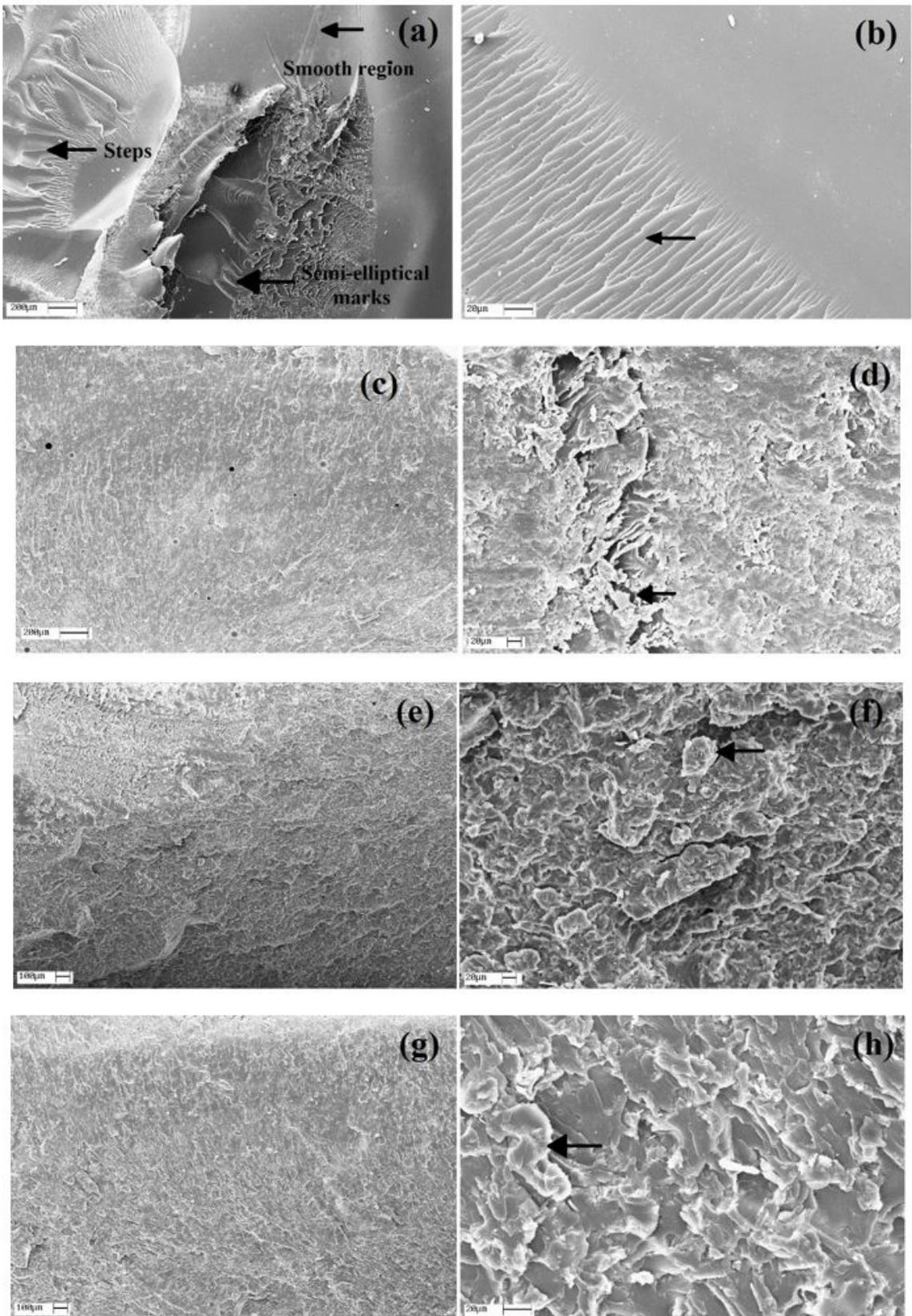


Figure 11. SEM micrographs of resin and nanocomposite (a) and (b) neat epoxy; (c) and (d) 4.0% CNCs; (e) and (f) 5.5% CNCs; and (g) and (h) 7.0% CNCs.

the mechanical properties, we can state that, during the deformation, the CNCs reinforced the system and increased the elastic modulus, but accelerated the fracture by acting as point defects.

4. Conclusions

The CNCs obtained from microcrystalline cellulose using the acid hydrolysis method presented a high degree of crystallinity, with around 82.7% of the majority being cellulose I with dimensions of length and diameter of (142 ± 36) nm and (11 ± 2.5) nm, respectively, which resulted in an aspect ratio of 12.5. This fibrous morphology led to the calculation of the volume fraction percolation threshold of 5.5%. Analysis of the epoxy/CNC nanocomposites showed that the addition of CNCs caused minor changes in the cure conversion and in the thermal properties. The mechanical tensile tests showed an increase in elastic modulus, but the expected abrupt increase over the percolation threshold was not observed. The Halpin-Tsai modulus of elasticity prediction model was applied and showed coherence in the curve tendency, though the experimental results were lower than the prediction, which was attributed to the lack of dispersion of the CNCs and the weak interaction between the phases. Impact resistance and the flexural modulus showed decreases when compared to pure resin. The lack of a better reinforcing effect may be explained by the hydrophilic nature of CNCs, which cause them to have a poor interaction with the epoxy matrix and/or by the lyophilized CNC aggregation, which shows that the applied dispersion process was not capable of uniformly dispersing the CNCs in the matrix.

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